Information From Differential Scanning Calorimetry

The goal is to find two parameters, which, when plotted one against the other, will result in a straight line. From the slope of such a line, some important parameters of the process could be calculated (for instance the overall effective activation energy E or the order of reaction n).

The fraction crystallized a in terms of nucleation rate J and crystal growth rate G is:

$$\mathbf{a} = l - exp\left[-g\int_{0}^{t} J_{o}\left(\int_{t'}^{t} Gdt\right)^{m} dt'\right]$$
(1)

For interface-controlled growth or diffusion controlled growth with *G* independent of time, m=1,2 and 3 depending on the dimension of growth. For diffusion controlled growth where $G \sim t^{-1/2} m = 1/2$, 1, 3/2. +1

For anisotropic growth $\prod_i \int G_i dt_i$

For constant J, G $\mathbf{a} = 1 - exp(-gJ_oG^mt^n), \quad n=m+1$ $\mathbf{a} = 1 - exp[-Kt^n]$ (2) $K = K_o exp\left(-\frac{E}{RT}\right)$ In general neither the activation energy E , nor the activation energy for lin

In general neither the activation energy E_N nor the activation energy for linear crystallization E_G are constant. As the process takes place in a narrow temperature region they are taken as effective values in this region.

$$E = E_n + mE_G$$

Interpretations of results: $T=T_o+qt$

Ozawa method to determine n

$$\boldsymbol{a} = 1 - \exp\left[-K\left(\frac{T - T_o}{q}\right)^n\right]$$
(3)

Taking twice the logarithm

 $\frac{d[ln(-ln(1-a))]}{d \ln q}\Big|_{T} = -n$ Here **a** is obtained at the same temperature from a number of crystallization experiments taken at different heating rates.

All other methods involve as a first step differentiation of eq.(2) with respect to time

Piloyan-Borchardt

$$\dot{\mathbf{a}} = (l - \mathbf{a})nKt^{m} \left(l + \frac{\dot{K}}{K} \right)$$

$$\dot{\mathbf{k}} = \frac{dK}{dT} \frac{dT}{dt} = q \frac{d}{dT} \left[K_{o} exp\left(-\frac{E}{RT} \right) \right] = \frac{qEK_{o}}{RT^{2}} exp\left(-\frac{E}{RT} \right)$$

$$\dot{\mathbf{a}} = (l - \mathbf{a})nKt^{m} (l + bt) \qquad ; \qquad b = \frac{qE}{RT^{2}}$$

$$(***)$$

If $T_o << T$ than $at \gg E/RT$

assumption !!?? *E*/*RT* << 1 !!??

$$\cdot \mathbf{a} \approx (l - \mathbf{a}) n K t^{m}$$

Dependence of \dot{x} on **a** and *t* assumption: It is possible to define

$$\mathbf{a} = k(x)h(T)$$

The time can be expressed in terms of a as:

$$t = \left[\frac{-\ln(1-a)}{K}\right]^{1/n} \qquad ; \qquad t = \frac{T-T_o}{q}$$

Coats-Redfern-Sestak method determines activation energy

Assumes that $k(\boldsymbol{a}) = (1 - \boldsymbol{a})^n$ from $\dot{\boldsymbol{a}} = k(\boldsymbol{a})K a^{-\frac{E}{RT}}$

from
$$\boldsymbol{a} = k(\boldsymbol{a})K_o e^{-RT}$$

by rearranging the above expression and integrating

 $\int_{0}^{X'} \frac{d\mathbf{a}}{k(\mathbf{a})} = K_{o} \int_{0}^{t'} e^{-\frac{E}{RT}} dt \equiv U(\mathbf{a}')$ The function $U(\mathbf{a}')$ is independent on the heating

rate used to obtain the crystallized fraction a'

The time integral is transformed to temperature integral

$$U(\mathbf{a}') = \frac{K_o}{q} \int_{T_o}^{T''} e^{-\frac{E}{RT}} dT = \frac{K_o E}{Rq} \int_{y_o}^{y''} \frac{e^{-y}}{y^2} dy \quad ; \quad y = \frac{E}{RT}$$
(*)

If we start at $T_o << T'$ (below T_g so that no crystallization takes place in this region we may assume $T_o @0$, *i.e.* $y_o = \mathbf{Y}$

Exponent integral function

$$\int \frac{e^{-y}}{y^2} dy = -\frac{e^{-y}}{y} + Ei(y)$$

$$E_i(y) = \frac{e^{-y}}{y} \left(1 - \frac{l!}{y} + \frac{2!}{y^2} \dots + \frac{(-1)^n n!}{y^n} \right)$$

$$Ei(y) = -\mathbf{g} - \ln y + \left(\frac{y}{1 \cdot 1!} - \frac{y^2}{2 \cdot 2!} + \frac{y^3}{3 \cdot 3!} - \dots \right) \quad , \gamma = 0.5772$$

for y' >> 1 the integral (*) becomes

$$\int_{-\infty}^{y'} \frac{e^{-y}}{y^2} dy \approx -\frac{e^{-{y'}^2}}{{y'}^2}$$

If $k(\mathbf{a}) \approx (1-\mathbf{a})[-\ln(1-\mathbf{a})]^{n-1/n}$
then $U(\mathbf{a}') = [-\ln(1-\mathbf{a}')]^{1/n} = \frac{K_o RT'^2}{Eq} e^{-\frac{E}{RT'}}$

Essential is that for a given \mathbf{a}' , $U(\mathbf{a}')=const$

$$\frac{K_o RT'^2}{Eq} e^{-\frac{E}{RT}} = const$$

$$ln \frac{T'^2}{q} - \frac{E}{RT'} = Const$$
This is known as Ozawa-Chen method

Ozawa used a simpler approximation and find coordinates ln q against 1/T'.

If a fixed **a**' is determined in a series of exotherms at different heating rates, the plot of $ln T^{2}/q vs 1/T$ ' should be a straight line with a slope E/R.

Derivation of Coats-Sestac-Redfern for E/RT >> 1

From Eq.(***) , since $qt/T \sim 1$

$$\dot{\boldsymbol{a}} = (1-\boldsymbol{a})nKt^m \frac{qE}{RT^2}$$

$$\int_{0}^{X'} \frac{d\boldsymbol{a}}{(l-\boldsymbol{a})\ln(l-\boldsymbol{a})} = \ln[-\ln(l-\boldsymbol{a})] = \frac{E}{R} \int_{0}^{T'} \frac{dT}{T^2} = -\frac{E}{RT'}$$

Bennet has shown that at temperature of the peak T_p the degree of transformation $a_p \gg 0.63$ DOES NOT DEPEND ON HEATING RATE OR THE ORDER OF THE REACTION

$$\boldsymbol{a}(t) = 1 - exp\left\{-c_g \int_0^t J(t') \left[\int_0^{t-t'} G(t'') dt''\right]^d dt'\right\}$$

This is the evolution of the crystallized fraction of the volume. It is controlled by two basic parameters – the crystallite nucleation and growth rates J and G

Growth	Shape	Cg
1D	Needle	2A ₀
2D	Disk	₽ H _o
2D	Square prism	$4H_o$
3D	Sphere	4 p /3
3D	cube	8

 A_o – constant cross section area of needle; H_o constant thickness of the prism

H. Yinnon, D. Uhlmann, J. Non Cryst Sol. 54 (1983) 253